

A

Seminar report

On

**Hydrology**

Submitted in partial fulfillment of the requirement for the award of degree  
Of Civil

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## Preface

I have made this report file on the topic **Hydrology**; I have tried my best to elucidate all the relevant detail to the topic to be included in the report. While in the beginning I have tried to give a general view about this topic.

My efforts and wholehearted co-corporation of each and everyone has ended on a successful note. I express my sincere gratitude to .....who assisting me throughout the preparation of this topic. I thank him for providing me the reinforcement, confidence and most importantly the track for the topic whenever I needed it.

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## **Acknowledgement**

I would like to thank respected Mr..... and Mr. ....for giving me such a wonderful opportunity to expand my knowledge for my own branch and giving me guidelines to present a seminar report. It helped me a lot to realize of what we study for.

Secondly, I would like to thank my parents who patiently helped me as i went through my work and helped to modify and eliminate some of the irrelevant or un-necessary stuffs.

Thirdly, I would like to thank my friends who helped me to make my work more organized and well-stacked till the end.

Next, I would thank Microsoft for developing such a wonderful tool like MS Word. It helped my work a lot to remain error-free.

Last but clearly not the least, I would thank The Almighty for giving me strength to complete my report on time.

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- Introduction
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- Applications
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- Project Analysis
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## Introduction

Engineering or applied hydrology – a study concerned with engineering application like design dam, our seminar given realistic case study (of catchment) in west bank. In our seminar we want to calculate the peak flow that produced from the excess rainfall at the area that we want to design the Dam.



## Precipitation

The atmospheric air always contains moisture. Evaporation from the oceans is the major source (about 90%) of the atmospheric moisture for precipitation. Continental evaporation contributes only about 10% of the atmospheric moisture for precipitation. The atmosphere contains the moisture even on days of bright sun-shine. However, for the occurrence of precipitation, some mechanism is required to cool the atmospheric air sufficiently to bring it to (or near) saturation.

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## Applications

- Determining the water balance of a region.
- Determining the agricultural water balance.
- Designing riparian restoration projects.
- Mitigating and predicting flood, landslide and drought risk.
- Real-time flood forecasting and flood warning.
- Designing irrigation schemes and managing agricultural productivity.
- Part of the hazard module in catastrophe modeling.
- Providing drinking water.
- Designing dams for water supply or hydroelectric power generation.
- Designing bridges.
- Designing sewers and urban drainage system.
- Analyzing the impacts of antecedent moisture on sanitary sewer systems.
- Predicting geomorphologic changes, such as erosion or sedimentation.
- Assessing the impacts of natural and anthropogenic environmental change on water resources.
- Assessing contaminant transport risk and establishing environmental policy guidelines.



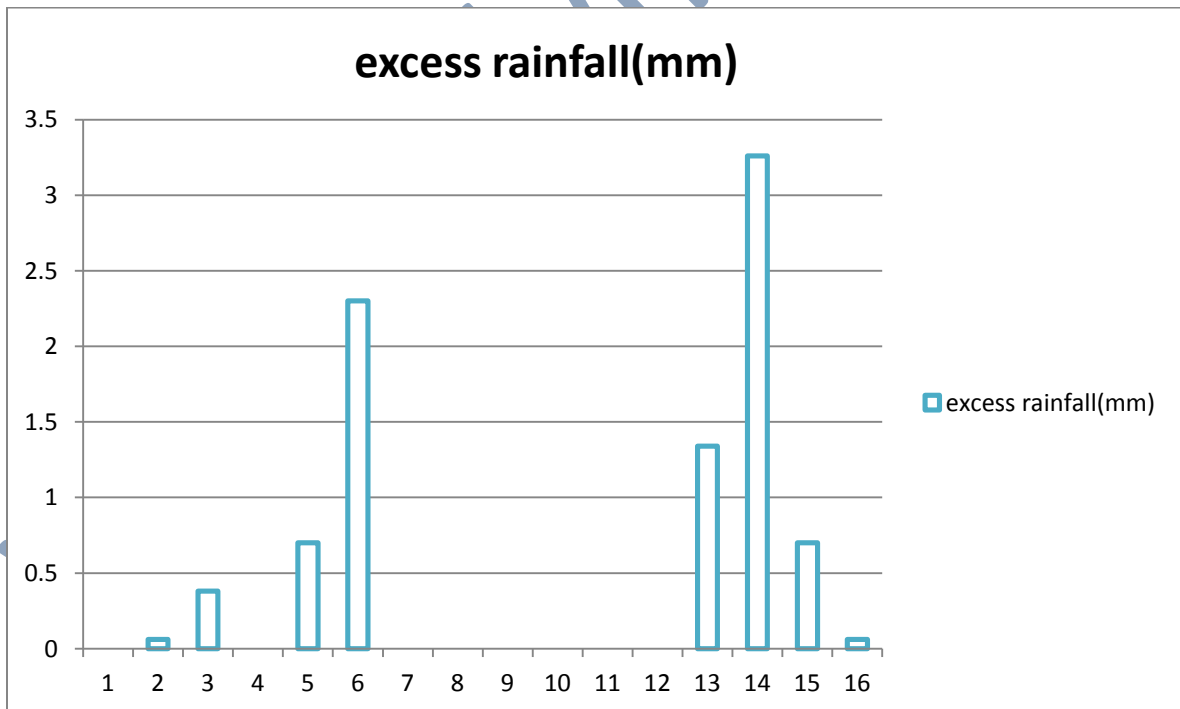
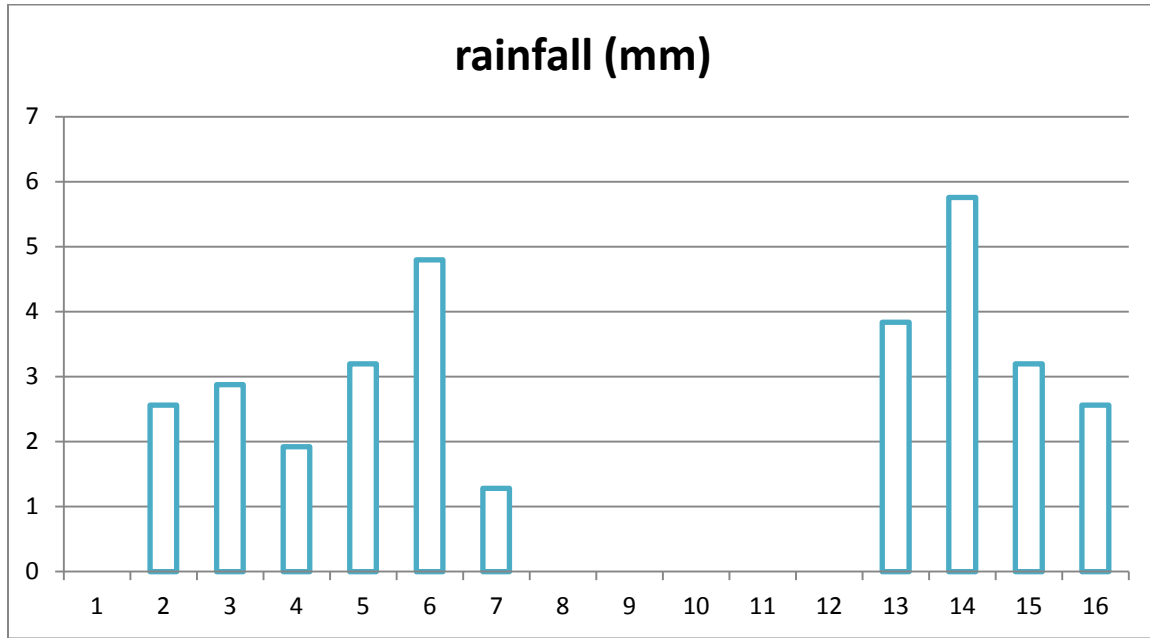
## Project Analysis

To estimate the volume, calculate each value for each hour of total rainfall by multiplying the percentage of rainfall by total amount of rainfall (32mm). Calculate the excess rainfall from the total rainfall by subtracting the losses ( $\Phi$ -index which 2.5mm/hr) from each value for each hour of total rainfall which is not less than 2.5mm/hr.

Data analysis

| time (hr) | rainfall(%) | R (mm) | rainfall%*R =<br>rainfall(mm) | $\phi$ -index     | excess<br>rainfall(mm) |
|-----------|-------------|--------|-------------------------------|-------------------|------------------------|
| 1         | 0           | 32     | 0                             | 2.5               | 0                      |
| 2         | 8           | 32     | 2.56                          | 2.5               | 0.06                   |
| 3         | 9           | 32     | 2.88                          | 2.5               | 0.38                   |
| 4         | 6           | 32     | 1.92                          | 2.5               | 0                      |
| 5         | 10          | 32     | 3.2                           | 2.5               | 0.7                    |
| 6         | 15          | 32     | 4.8                           | 2.5               | 2.3                    |
| 7         | 4           | 32     | 1.28                          | 2.5               | 0                      |
| 8         | 0           | 32     | 0                             | 2.5               | 0                      |
| 9         | 0           | 32     | 0                             | 2.5               | 0                      |
| 10        | 0           | 32     | 0                             | 2.5               | 0                      |
| 11        | 0           | 32     | 0                             | 2.5               | 0                      |
| 12        | 0           | 32     | 0                             | 2.5               | 0                      |
| 13        | 12          | 32     | 3.84                          | 2.5               | 1.34                   |
| 14        | 18          | 32     | 5.76                          | 2.5               | 3.26                   |
| 15        | 10          | 32     | 3.2                           | 2.5               | 0.7                    |
| 16        | 8           | 32     | 2.56                          | 2.5               | 0.06                   |
| sum       |             |        | 32                            | depth of DRO<br>= | 8.8                    |





- Estimate the volume of direct runoff and volume of infiltration (in million cubic meters) for 1 and 2 sub-catchments.

$$V = d * A$$

|                           |
|---------------------------|
| depth under $\phi$ -index |
| 23.2                      |
| depth of excess rainfall  |
| 8.8                       |

| Sub. | Area(KM <sup>2</sup> ) | vol. of infil.m <sup>3</sup> | vol. of dir. runoff m <sup>3</sup> | vol. of infil. Mm <sup>3</sup> | vol. of dir.runoff Mm <sup>3</sup> |
|------|------------------------|------------------------------|------------------------------------|--------------------------------|------------------------------------|
| 1    | 84                     | 1948800                      | 739200                             | 1.9488                         | 0.7392                             |
| 2    | 64                     | 1484800                      | 563200                             | 1.4848                         | 0.5632                             |

- We calculate the hydrograph then estimate the volume of direct runoff from hydrograph (Compare your results with those of part 1.) Will be discussed in discussion and conclusion part(1).

We have 1 h.u.H , and the storm divide by 1 hr so, we don't need convert between D h.u.H.

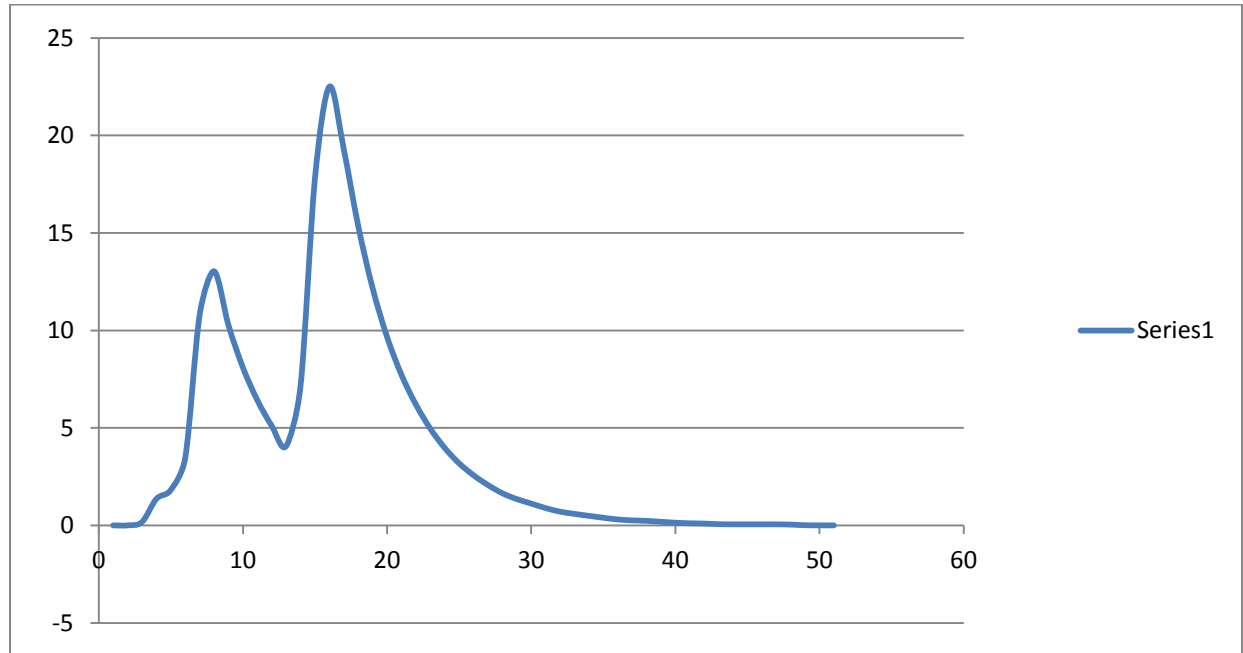
for sub-catchment 1 and 2 as follow:

**For 1:**

| hydrograph for 1 |        |        |       |       |    |    |    |    |        |
|------------------|--------|--------|-------|-------|----|----|----|----|--------|
| time             | Q1     | Q2     | Q3    | Q4    | Q5 | Q6 | Q7 | Q8 | sum    |
| 1                |        |        |       |       |    |    |    |    | 0      |
| 2                | 0      |        |       |       |    |    |    |    | 0      |
| 3                | 0.1746 | 0      |       |       |    |    |    |    | 0.1746 |
| 4                | 0.2556 | 1.1058 |       |       |    |    |    |    | 1.3614 |
| 5                | 0.201  | 1.6188 | 0     |       |    |    |    |    | 1.8198 |
| 6                | 0.1584 | 1.273  | 2.037 | 0     |    |    |    |    | 3.4684 |
| 7                | 0.1254 | 1.0032 | 2.982 | 6.693 |    |    |    |    | 10.804 |
| 8                | 0.0996 | 0.7942 | 2.345 | 9.798 |    |    |    |    | 13.03  |

|    |        |        |       |       |        |        |       |        |        |
|----|--------|--------|-------|-------|--------|--------|-------|--------|--------|
|    |        |        |       |       |        |        |       |        | 7      |
| 9  | 0.0792 | 0.6308 | 1.848 | 7.705 |        |        |       |        | 10.263 |
| 10 | 0.0636 | 0.5016 | 1.463 | 6.072 |        |        |       |        | 8.1002 |
| 11 | 0.051  | 0.4028 | 1.162 | 4.807 |        |        |       |        | 6.4228 |
| 12 | 0.0408 | 0.323  | 0.924 | 3.818 |        |        |       |        | 5.1058 |
| 13 | 0.0324 | 0.2584 | 0.742 | 3.036 | 0      |        |       |        | 4.0688 |
| 14 | 0.0264 | 0.2052 | 0.595 | 2.438 | 3.8994 | 0      |       |        | 7.164  |
| 15 | 0.021  | 0.1672 | 0.476 | 1.955 | 5.7084 | 9.4866 | 0     |        | 17.814 |
| 16 | 0.0168 | 0.133  | 0.378 | 1.564 | 4.489  | 13.888 | 2.037 | 0      | 22.505 |
| 17 | 0.0138 | 0.1064 | 0.308 | 1.242 | 3.5376 | 10.921 | 2.982 | 0.1746 | 19.285 |
| 18 | 0.0114 | 0.0874 | 0.245 | 1.012 | 2.8006 | 8.6064 | 2.345 | 0.2556 | 15.363 |
| 19 | 0.009  | 0.0722 | 0.196 | 0.805 | 2.2244 | 6.8134 | 1.848 | 0.201  | 12.169 |
| 20 | 0.0072 | 0.057  | 0.161 | 0.644 | 1.7688 | 5.4116 | 1.463 | 0.1584 | 9.671  |
| 21 | 0.006  | 0.0456 | 0.133 | 0.529 | 1.4204 | 4.3032 | 1.162 | 0.1254 | 7.7246 |
| 22 | 0.0048 | 0.038  | 0.105 | 0.437 | 1.139  | 3.4556 | 0.924 | 0.0996 | 6.203  |
| 23 | 0.0042 | 0.0304 | 0.084 | 0.345 | 0.9112 | 2.771  | 0.742 | 0.0792 | 4.967  |
| 24 | 0.003  | 0.0266 | 0.07  | 0.276 | 0.7236 | 2.2168 | 0.595 | 0.0636 | 3.9746 |
| 25 | 0.0024 | 0.019  | 0.056 | 0.23  | 0.5896 | 1.7604 | 0.476 | 0.051  | 3.1844 |
| 26 | 0.0024 | 0.0152 | 0.049 | 0.184 | 0.469  | 1.4344 | 0.378 | 0.0408 | 2.5728 |
| 27 | 0.0018 | 0.0152 | 0.035 | 0.161 | 0.3752 | 1.141  | 0.308 | 0.0324 | 2.0696 |
| 28 | 0.0012 | 0.0114 | 0.028 | 0.115 | 0.3082 | 0.9128 | 0.245 | 0.0264 | 1.648  |
| 29 | 0.0012 | 0.0076 | 0.028 | 0.092 | 0.2546 | 0.7498 | 0.196 | 0.021  | 1.3502 |
| 30 | 0.0012 | 0.0076 | 0.021 | 0.092 | 0.201  | 0.6194 | 0.161 | 0.0168 | 1.12   |
| 31 | 0.0006 | 0.0076 | 0.014 | 0.069 | 0.1608 | 0.489  | 0.133 | 0.0138 | 0.8878 |
| 32 | 0.0006 | 0.0038 | 0.014 | 0.046 | 0.134  | 0.3912 | 0.105 | 0.0114 | 0.706  |
| 33 | 0.0006 | 0.0038 | 0.014 | 0.046 | 0.1072 | 0.326  | 0.084 | 0.009  | 0.5906 |
| 34 | 0.0006 | 0.0038 | 0.007 | 0.046 | 0.0938 | 0.2608 | 0.07  | 0.0072 | 0.489  |

|    |        |                                      |              |                 |        |        |       |        |            |
|----|--------|--------------------------------------|--------------|-----------------|--------|--------|-------|--------|------------|
|    |        |                                      |              |                 |        |        |       |        | 2          |
| 35 | 0.0006 | 0.0038                               | 0.007        | 0.023           | 0.067  | 0.2282 | 0.056 | 0.006  | 0.3916     |
| 36 | 0.0006 | 0.0038                               | 0.007        | 0.023           | 0.0536 | 0.163  | 0.049 | 0.0048 | 0.3048     |
| 37 | 0      | 0.0038                               | 0.007        | 0.023           | 0.0536 | 0.1304 | 0.035 | 0.0042 | 0.257      |
| 38 |        | 0                                    | 0.007        | 0.023           | 0.0402 | 0.1304 | 0.028 | 0.003  | 0.2316     |
| 39 |        |                                      | 0.007        | 0.023           | 0.0268 | 0.0978 | 0.028 | 0.0024 | 0.185      |
| 40 |        |                                      | 0            | 0.023           | 0.0268 | 0.0652 | 0.021 | 0.0024 | 0.1384     |
| 41 |        |                                      |              | 0               | 0.0268 | 0.0652 | 0.014 | 0.0018 | 0.1078     |
| 42 |        |                                      |              |                 | 0.0134 | 0.0652 | 0.014 | 0.0012 | 0.0938     |
| 43 |        |                                      |              |                 | 0.0134 | 0.0326 | 0.014 | 0.0012 | 0.0612     |
| 44 |        |                                      |              |                 | 0.0134 | 0.0326 | 0.007 | 0.0012 | 0.0542     |
| 45 |        |                                      |              |                 | 0.0134 | 0.0326 | 0.007 | 0.0006 | 0.0536     |
| 46 |        |                                      |              |                 | 0.0134 | 0.0326 | 0.007 | 0.0006 | 0.0536     |
| 47 |        |                                      |              |                 | 0.0134 | 0.0326 | 0.007 | 0.0006 | 0.0536     |
| 48 |        |                                      |              |                 | 0      | 0.0326 | 0.007 | 0.0006 | 0.0402     |
| 49 |        |                                      |              |                 |        | 0      | 0.007 | 0.0006 | 0.0076     |
| 50 |        |                                      |              |                 |        |        | 0     | 0.0006 | 0.0006     |
| 51 |        |                                      |              |                 |        |        |       | 0      | 0          |
|    |        | <u>Vol.</u><br><u>dir.runof</u><br>f | 0.74923<br>2 | Mm <sup>3</sup> |        |        |       |        | 208.1<br>2 |



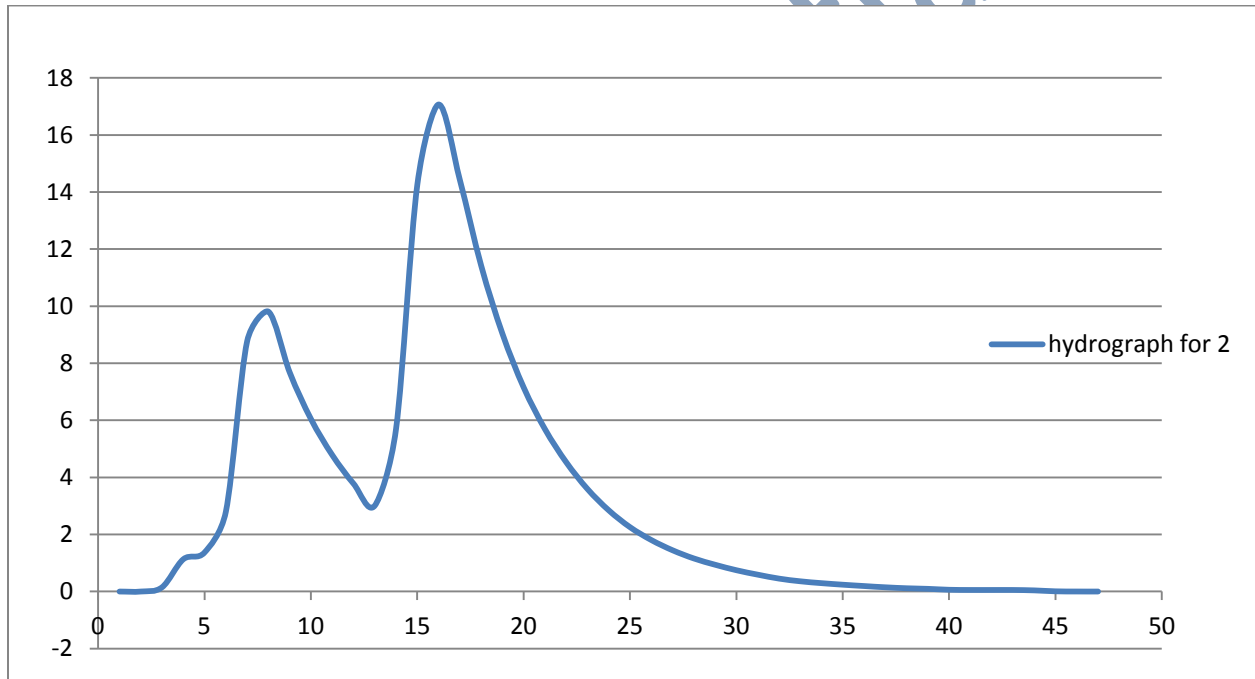
Hydrograph for sub-cat. 1

**For 2:**

| hydrograph for 2 |        |        |       |       |    |    |    |    |        |
|------------------|--------|--------|-------|-------|----|----|----|----|--------|
| time             | Q1     | Q2     | Q3    | Q4    | Q5 | Q6 | Q7 | Q8 | sum    |
| 1                |        |        |       |       |    |    |    |    | 0      |
| 2                | 0      |        |       |       |    |    |    |    | 0      |
| 3                | 0.1482 | 0      |       |       |    |    |    |    | 0.1482 |
| 4                | 0.1926 | 0.9386 |       |       |    |    |    |    | 1.1312 |
| 5                | 0.1506 | 1.2198 | 0     |       |    |    |    |    | 1.3704 |
| 6                | 0.1182 | 0.9538 | 1.729 | 0     |    |    |    |    | 2.801  |
| 7                | 0.0936 | 0.7486 | 2.247 | 5.681 |    |    |    |    | 8.7702 |
| 8                | 0.0738 | 0.5928 | 1.757 | 7.383 |    |    |    |    | 9.8066 |
| 9                | 0.0588 | 0.4674 | 1.379 | 5.773 |    |    |    |    | 7.6782 |
| 10               | 0.0468 | 0.3724 | 1.092 | 4.531 |    |    |    |    | 6.0422 |
| 11               | 0.0372 | 0.2964 | 0.861 | 3.588 |    |    |    |    | 4.7826 |

|    |        |        |       |       |        |        |       |        |        |
|----|--------|--------|-------|-------|--------|--------|-------|--------|--------|
| 12 | 0.0294 | 0.2356 | 0.686 | 2.829 |        |        |       |        | 3.78   |
| 13 | 0.0234 | 0.1862 | 0.546 | 2.254 | 0      |        |       |        | 3.0096 |
| 14 | 0.0186 | 0.1482 | 0.434 | 1.794 | 3.3098 | 0      |       |        | 5.7046 |
| 15 | 0.015  | 0.1178 | 0.343 | 1.426 | 4.3014 | 8.0522 | 0     |        | 14.255 |
| 16 | 0.012  | 0.095  | 0.273 | 1.127 | 3.3634 | 10.465 | 1.729 | 0      | 17.064 |
| 17 | 0.0096 | 0.076  | 0.217 | 0.897 | 2.6398 | 8.1826 | 2.247 | 0.1482 | 14.417 |
| 18 | 0.0078 | 0.0608 | 0.175 | 0.713 | 2.0904 | 6.4222 | 1.757 | 0.1926 | 11.419 |
| 19 | 0.006  | 0.0494 | 0.14  | 0.575 | 1.6482 | 5.0856 | 1.379 | 0.1506 | 9.0338 |
| 20 | 0.0048 | 0.038  | 0.112 | 0.46  | 1.3132 | 4.0098 | 1.092 | 0.1182 | 7.148  |
| 21 | 0.0036 | 0.0304 | 0.091 | 0.368 | 1.0452 | 3.1948 | 0.861 | 0.0936 | 5.6876 |
| 22 | 0.003  | 0.0228 | 0.07  | 0.299 | 0.8308 | 2.5428 | 0.686 | 0.0738 | 4.5282 |
| 23 | 0.0024 | 0.019  | 0.056 | 0.23  | 0.6566 | 2.0212 | 0.546 | 0.0588 | 3.59   |
| 24 | 0.0018 | 0.0152 | 0.042 | 0.184 | 0.5226 | 1.5974 | 0.434 | 0.0468 | 2.8438 |
| 25 | 0.0018 | 0.0114 | 0.035 | 0.138 | 0.4154 | 1.2714 | 0.343 | 0.0372 | 2.2532 |
| 26 | 0.0012 | 0.0114 | 0.028 | 0.115 | 0.335  | 1.0106 | 0.273 | 0.0294 | 1.8036 |
| 27 | 0.0012 | 0.0076 | 0.021 | 0.092 | 0.268  | 0.815  | 0.217 | 0.0234 | 1.4452 |
| 28 | 0.0006 | 0.0076 | 0.021 | 0.069 | 0.2144 | 0.652  | 0.175 | 0.0186 | 1.1582 |
| 29 | 0.0006 | 0.0038 | 0.014 | 0.069 | 0.1742 | 0.5216 | 0.14  | 0.015  | 0.9382 |
| 30 | 0.0006 | 0.0038 | 0.014 | 0.046 | 0.134  | 0.4238 | 0.112 | 0.012  | 0.7462 |
| 31 | 0.0006 | 0.0038 | 0.007 | 0.046 | 0.1072 | 0.326  | 0.091 | 0.0096 | 0.5912 |
| 32 | 0.0006 | 0.0038 | 0.007 | 0.023 | 0.0804 | 0.2608 | 0.07  | 0.0078 | 0.4534 |
| 33 | 0      | 0.0038 | 0.007 | 0.023 | 0.067  | 0.1956 | 0.056 | 0.006  | 0.3584 |
| 34 |        | 0      | 0.007 | 0.023 | 0.0536 | 0.163  | 0.042 | 0.0048 | 0.2934 |
| 35 |        |        | 0.007 | 0.023 | 0.0402 | 0.1304 | 0.035 | 0.0036 | 0.2392 |
| 36 |        |        | 0     | 0.023 | 0.0402 | 0.0978 | 0.028 | 0.003  | 0.192  |
| 37 |        |        |       | 0     | 0.0268 | 0.0978 | 0.021 | 0.0024 | 0.148  |
| 38 |        |        |       |       | 0.0268 | 0.0652 | 0.021 | 0.0018 | 0.1148 |
| 39 |        |        |       |       | 0.0134 | 0.0652 | 0.014 | 0.0018 | 0.0944 |
| 40 |        |        |       |       | 0.0134 | 0.0326 | 0.014 | 0.0012 | 0.0612 |

|    |  |   |              |                 |        |        |       |        |        |
|----|--|---|--------------|-----------------|--------|--------|-------|--------|--------|
| 41 |  |   |              |                 | 0.0134 | 0.0326 | 0.007 | 0.0012 | 0.0542 |
| 42 |  |   |              |                 | 0.0134 | 0.0326 | 0.007 | 0.0006 | 0.0536 |
| 43 |  |   |              |                 | 0.0134 | 0.0326 | 0.007 | 0.0006 | 0.0536 |
| 44 |  |   |              |                 | 0      | 0.0326 | 0.007 | 0.0006 | 0.0402 |
| 45 |  |   |              |                 |        | 0      | 0.007 | 0.0006 | 0.0076 |
| 46 |  |   |              |                 |        |        | 0     | 0.0006 | 0.0006 |
| 47 |  |   |              |                 |        |        |       | 0      | 0      |
|    |  | <u>Vol.</u><br><u>dir.runof</u><br><u>f</u> | 0.56200<br>3 | Mm <sup>3</sup> |        |        |       |        | 156.11 |

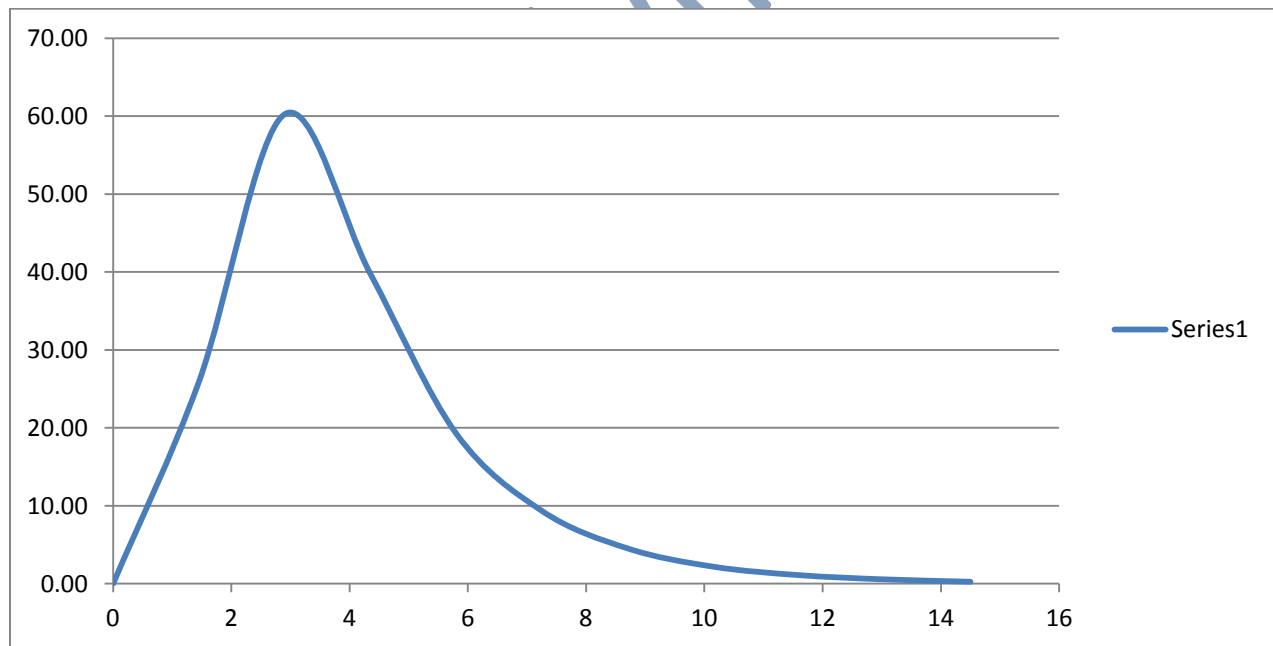


Hydrograph for sub-cat. 2

- We use the SCS method to derive a 1hr-UH using the SCS method (Compare your results with the given UHs.) Will be discussed in discussion and conclusion(2). By using SCS Dimensionless method unit hydrograph, this method is analyzed and illustrated in the next tables.

For 1:

| Assume<br>tc=4 hr |          | 1 h.u.h           |  | T/Tp | Q/Qp  | T (hr) | Q (m <sup>3</sup> /s) |
|-------------------|----------|-------------------|--|------|-------|--------|-----------------------|
| tr=1 hr           |          |                   |  | 0    | 0     | 0      | 0.00                  |
| Tp=               | 2.9      | hr                |  | 0.5  | 0.43  | 1.45   | 25.91                 |
| Tb=               | 7.743    | hr                |  | 1    | 1     | 2.9    | 60.25                 |
| Qp=               | 60.24828 | m <sup>3</sup> /s |  | 1.5  | 0.66  | 4.35   | 39.76                 |
|                   |          |                   |  | 2    | 0.32  | 5.8    | 19.28                 |
|                   |          |                   |  | 2.5  | 0.155 | 7.25   | 9.34                  |
|                   |          |                   |  | 3    | 0.075 | 8.7    | 4.52                  |
|                   |          |                   |  | 3.5  | 0.036 | 10.15  | 2.17                  |
|                   |          |                   |  | 4    | 0.018 | 11.6   | 1.08                  |
|                   |          |                   |  | 4.5  | 0.009 | 13.05  | 0.54                  |
|                   |          |                   |  | 5    | 0.004 | 14.5   | 0.24                  |

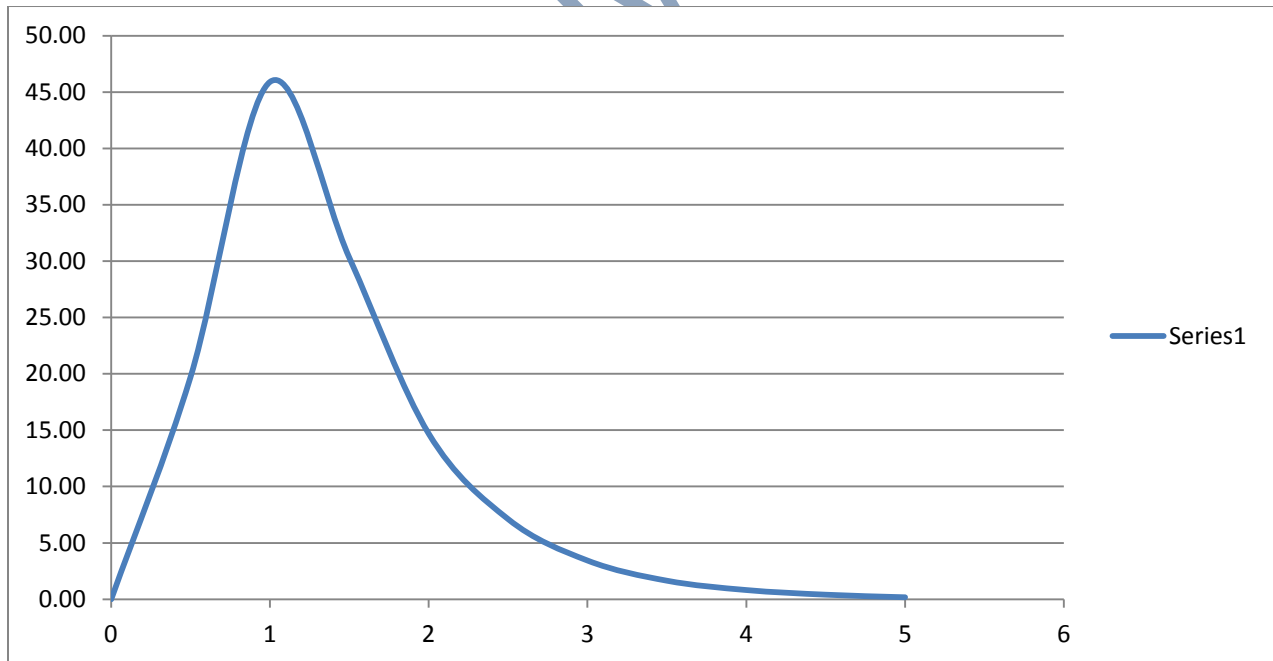


1hr-UH using the SCS method for 1

For 2:



| Assume<br>tc=4 hr |          | 1 h.u.h           |  | T/Tp | Q/Qp  | T (hr) | Q (m <sup>3</sup> /s) |
|-------------------|----------|-------------------|--|------|-------|--------|-----------------------|
| tr=1 hr           |          |                   |  | 0    | 0     | 0      | 0.00                  |
| Tp=               | 2.9      | hr                |  | 0.5  | 0.43  | 1.45   | 19.74                 |
| Tb=               | 7.743    | hr                |  | 1    | 1     | 2.9    | 45.90                 |
| Qp=               | 45.90345 | m <sup>3</sup> /s |  | 1.5  | 0.66  | 4.35   | 30.30                 |
|                   |          |                   |  | 2    | 0.32  | 5.8    | 14.69                 |
|                   |          |                   |  | 2.5  | 0.155 | 7.25   | 7.12                  |
|                   |          |                   |  | 3    | 0.075 | 8.7    | 3.44                  |
|                   |          |                   |  | 3.5  | 0.036 | 10.15  | 1.65                  |
|                   |          |                   |  | 4    | 0.018 | 11.6   | 0.83                  |
|                   |          |                   |  | 4.5  | 0.009 | 13.05  | 0.41                  |
|                   |          |                   |  | 5    | 0.004 | 14.5   | 0.18                  |



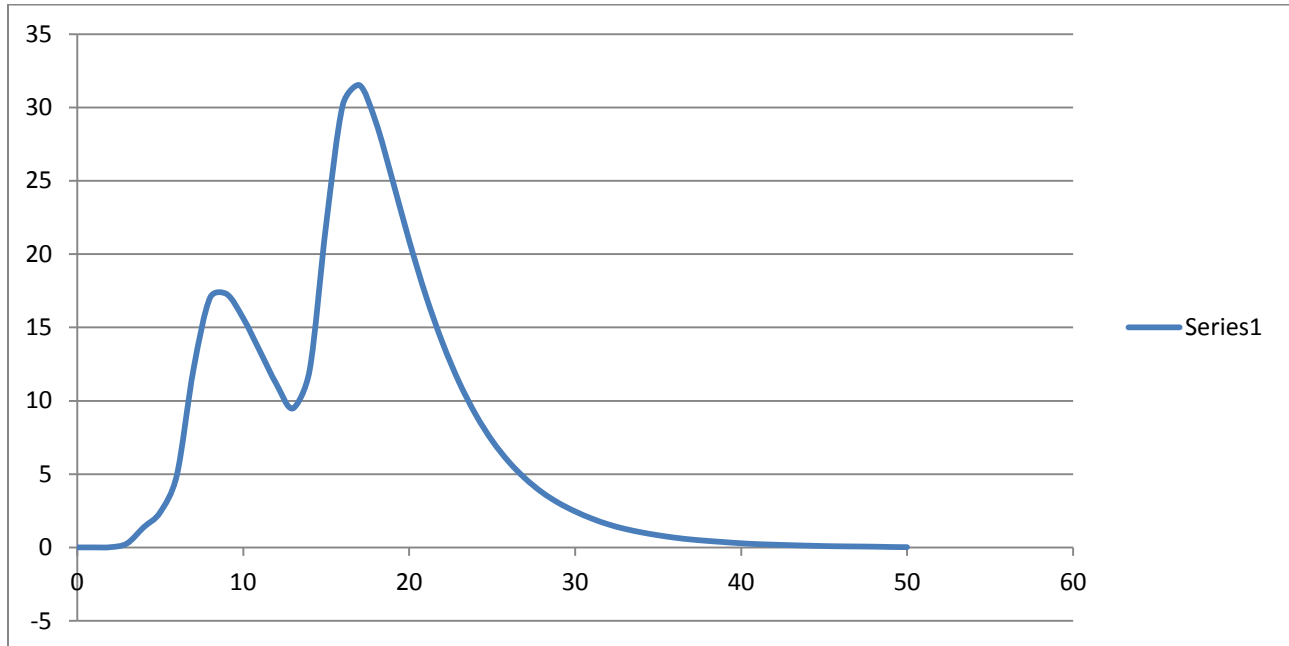
1hr-UH using the SCS method for 2

- we calculate the hydrograph after 3km because we want to design the dam as follow, first we calculate the constant for the equation

|              |      |
|--------------|------|
| k=           | 2    |
| x =          | 0.2  |
| t            | 1    |
| Kx=          | 0.4  |
| k-<br>kx+.5t | 2.1  |
|              |      |
| C0           | 0.05 |
| C1           | 0.43 |
| C2           | 0.52 |
|              | 1    |

| sub   | 1        | 2        |                 |          |          |          |          |
|-------|----------|----------|-----------------|----------|----------|----------|----------|
| t(hr) | Q1(m3/s) | Q2(m3/s) | $\Sigma(Q1+Q2)$ | $C_0I_2$ | $C_1I_1$ | $C_2O_1$ | $O_2$    |
| 0     | 0        | 0        | 0               | 0        |          |          | 0        |
| 1     | 0        | 0        | 0               | 0        | 0        | 0        | 0        |
| 2     | 0.1746   | 0.1482   | 0.3228          | 0.01614  | 0        | 0        | 0.01614  |
| 3     | 1.3614   | 1.1312   | 2.4926          | 0.12463  | 0.138804 | 0.008393 | 0.271827 |
| 4     | 1.8198   | 1.3704   | 3.1902          | 0.15951  | 1.071818 | 0.14135  | 1.372678 |
| 5     | 3.4684   | 2.801    | 6.2694          | 0.31347  | 1.371786 | 0.713793 | 2.399049 |
| 6     | 10.8036  | 8.7702   | 19.5738         | 0.97869  | 2.695842 | 1.247505 | 4.922037 |
| 7     | 13.0368  | 9.8066   | 22.8434         | 1.14217  | 8.416734 | 2.559459 | 12.11836 |
| 8     | 10.263   | 7.6782   | 17.9412         | 0.89706  | 9.822662 | 6.301549 | 17.02127 |
| 9     | 8.1002   | 6.0422   | 14.1424         | 0.70712  | 7.714716 | 8.851061 | 17.2729  |
| 10    | 6.4228   | 4.7826   | 11.2054         | 0.56027  | 6.081232 | 8.981906 | 15.62341 |
| 11    | 5.1058   | 3.78     | 8.8858          | 0.44429  | 4.818322 | 8.124172 | 13.38678 |
| 12    | 4.0688   | 3.0096   | 7.0784          | 0.35392  | 3.820894 | 6.961128 | 11.13594 |
| 13    | 7.164    | 5.7046   | 12.8686         | 0.64343  | 3.043712 | 5.79069  | 9.477832 |
| 14    | 17.8142  | 14.2554  | 32.0696         | 1.60348  | 5.533498 | 4.928473 | 12.06545 |
| 15    | 22.5054  | 17.064   | 39.5694         | 1.97847  | 13.78993 | 6.274034 | 22.04243 |
| 16    | 19.2854  | 14.4172  | 33.7026         | 1.68513  | 17.01484 | 11.46206 | 30.16204 |
| 17    | 15.3634  | 11.4188  | 26.7822         | 1.33911  | 14.49212 | 15.68426 | 31.51549 |
| 18    | 12.169   | 9.0338   | 21.2028         | 1.06014  | 11.51635 | 16.38805 | 28.96454 |
| 19    | 9.671    | 7.148    | 16.819          | 0.84095  | 9.117204 | 15.06156 | 25.01971 |
| 20    | 7.7246   | 5.6876   | 13.4122         | 0.67061  | 7.23217  | 13.01025 | 20.91303 |

|    |        |        |         |         |          |          |          |
|----|--------|--------|---------|---------|----------|----------|----------|
| 21 | 6.203  | 4.5282 | 10.7312 | 0.53656 | 5.767246 | 10.87478 | 17.17858 |
| 22 | 4.967  | 3.59   | 8.557   | 0.42785 | 4.614416 | 8.932863 | 13.97513 |
| 23 | 3.9746 | 2.8438 | 6.8184  | 0.34092 | 3.67951  | 7.267067 | 11.2875  |
| 24 | 3.1844 | 2.2532 | 5.4376  | 0.27188 | 2.931912 | 5.869498 | 9.07329  |
| 25 | 2.5728 | 1.8036 | 4.3764  | 0.21882 | 2.338168 | 4.718111 | 7.275099 |
| 26 | 2.0696 | 1.4452 | 3.5148  | 0.17574 | 1.881852 | 3.783051 | 5.840643 |
| 27 | 1.648  | 1.1582 | 2.8062  | 0.14031 | 1.511364 | 3.037135 | 4.688809 |
| 28 | 1.3502 | 0.9382 | 2.2884  | 0.11442 | 1.206666 | 2.43818  | 3.759266 |
| 29 | 1.12   | 0.7462 | 1.8662  | 0.09331 | 0.984012 | 1.954819 | 3.032141 |
| 30 | 0.8878 | 0.5912 | 1.479   | 0.07395 | 0.802466 | 1.576713 | 2.453129 |
| 31 | 0.706  | 0.4534 | 1.1594  | 0.05797 | 0.63597  | 1.275627 | 1.969567 |
| 32 | 0.5906 | 0.3584 | 0.949   | 0.04745 | 0.498542 | 1.024175 | 1.570167 |
| 33 | 0.4892 | 0.2934 | 0.7826  | 0.03913 | 0.40807  | 0.816487 | 1.263687 |
| 34 | 0.3916 | 0.2392 | 0.6308  | 0.03154 | 0.336518 | 0.657117 | 1.025175 |
| 35 | 0.3048 | 0.192  | 0.4968  | 0.02484 | 0.271244 | 0.533091 | 0.829175 |
| 36 | 0.257  | 0.148  | 0.405   | 0.02025 | 0.213624 | 0.431171 | 0.665045 |
| 37 | 0.2316 | 0.1148 | 0.3464  | 0.01732 | 0.17415  | 0.345823 | 0.537293 |
| 38 | 0.185  | 0.0944 | 0.2794  | 0.01397 | 0.148952 | 0.279393 | 0.442315 |
| 39 | 0.1384 | 0.0612 | 0.1996  | 0.00998 | 0.120142 | 0.230004 | 0.360126 |
| 40 | 0.1078 | 0.0542 | 0.162   | 0.0081  | 0.085828 | 0.187265 | 0.281193 |
| 41 | 0.0938 | 0.0536 | 0.1474  | 0.00737 | 0.06966  | 0.146221 | 0.223251 |
| 42 | 0.0612 | 0.0536 | 0.1148  | 0.00574 | 0.063382 | 0.11609  | 0.185212 |
| 43 | 0.0542 | 0.0402 | 0.0944  | 0.00472 | 0.049364 | 0.09631  | 0.150394 |
| 44 | 0.0536 | 0.0076 | 0.0612  | 0.00306 | 0.040592 | 0.078205 | 0.121857 |
| 45 | 0.0536 | 0.0006 | 0.0542  | 0.00271 | 0.026316 | 0.063366 | 0.092392 |
| 46 | 0.0536 | 0      | 0.0536  | 0.00268 | 0.023306 | 0.048044 | 0.07403  |
| 47 | 0.0402 | 0      | 0.0402  | 0.00201 | 0.023048 | 0.038495 | 0.063553 |
| 48 | 0.0076 | 0      | 0.0076  | 0.00038 | 0.017286 | 0.033048 | 0.050714 |
| 49 | 0.0006 | 0      | 0.0006  | 0.00003 | 0.003268 | 0.026371 | 0.029669 |
| 50 | 0      | 0      | 0       | 0       | 0.000258 | 0.015428 | 0.015686 |
|    |        |        |         |         |          | total=   | 364.215  |



Hydrograph after 3 Km that produce from storm

**Discussion and Conclusion:**

(1) From part 1, the volume of direct runoff and volume of infiltration (in million cubic meters) for 1 and 2 sub-catchments.

| Sub. | vol. of dir.runoff<br>Mm <sup>3</sup> |
|------|---------------------------------------|
| 1    | 0.7392                                |
| 2    | 0.5632                                |

From part 3, the volume of direct runoff from hydrograph (in million cubic meters) for 1 and 2 sub-catchments.

| Sub. | vol. of dir.runoff<br>Mm <sup>3</sup> |
|------|---------------------------------------|
| 1    | 0.749232                              |
| 2    | 0.562003                              |

By comparing between it, approximate equal but there very small error , this inequality is because the depth of the given 1-mm UH for each catchment doesn't equal 1-mm.

(2) Compare between derive a 1hr-UH using the SCS method and results with the given UHs.

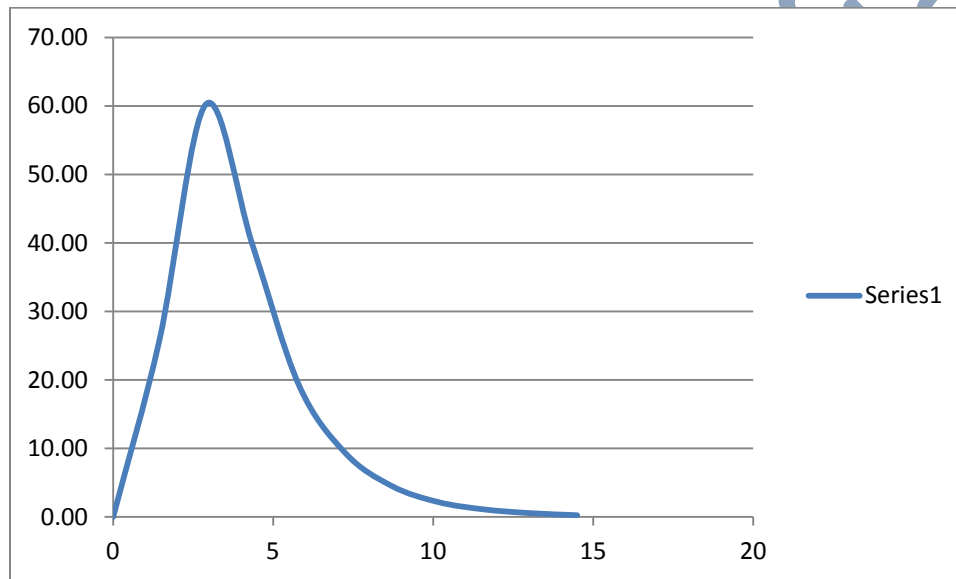
From 1hr-UH using the SCS method:

Catchment 1:

|     |          |                   |
|-----|----------|-------------------|
| Tp= | 2.9      | hr                |
| Tb= | 7.743    | hr                |
| Qp= | 60.24828 | m <sup>3</sup> /s |

From given 1hr-UH

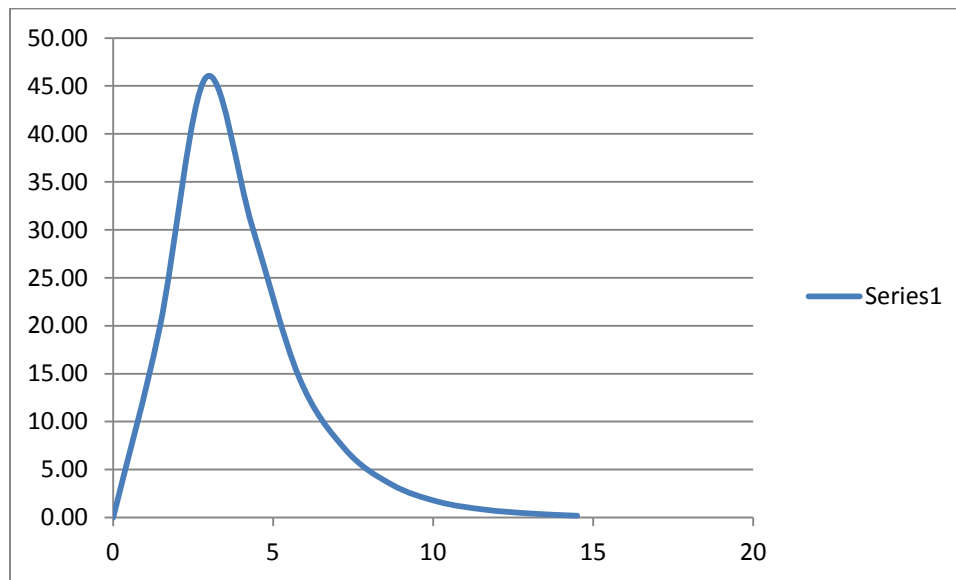
As we shown 1hr-UH



The peak of the given 1-hr UH and the peak of the estimated 1-hr UH by SCS method are the same for each catchment. But the time base different from those in the given 1-hr UH.

The time base of 1 catchment for the given 1-hr UH is 35 hrs, but for the estimated 1-hr UH by SCS method is 14.5 hrs.

Catchment 2:



The peak of the given 1-hr UH and the peak of the estimated 1-hr UH by SCS method are the same for each catchment. But the time base different from those in the given 1-hr UH.

The time base of 2 catchment for the given 1-hr UH is 31 hrs, but for the estimated 1-hr UH by SCS method is 14.5 hrs.

Also, note that the two time base for the estimated 1-hr UHs by SCS method for the two catchments are the same and equal 10 hrs.

## Conclusion

The Hydrologic Cycle is constantly happening all around us each and every day and is an essential part of life. It is necessary so that we have shade from clouds, to water our plants with the falling rain, and for fish to swim in. I hope you found this unit interesting and enjoyable, and appreciate water even more!

To learn more about water and the Hydrologic Cycle refer to the links on the websites given, look in your school library, or ask your teacher to direct you to other resources.

## References

- [www.google.com](http://www.google.com)
- [www.wikipedia.com](http://www.wikipedia.com)
- [www.studymafia.org](http://www.studymafia.org)

WWW.Studymafia.Org